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Contribution from the Lawrence Radiation Laboratory and Department of Chemistry, University of California, Berkeley, California 94720

The Atomic Parameters in the Lanthanum Trifluoride Structure¹

BY ALLAN ZALKIN, DAVID H. TEMPLETON, AND TED E. HOPKINS

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Crystals of LaF₃ exhibit a structure which is typical of numerous trifluorides of lanthanide and actinide elements. In 1931 Oftedal² suggested a structure, based on a study of crystals of the mineral tysonite, with the assumption that the space group is P6₃/mcm, but with atomic coordinates which correspond almost to the symmetry P6₃/mmc with a smaller unit cell. The evidence for the larger cell is the presence of weak reflections which may easily escape detection in powder diagrams. Schlyter³ failed to see these reflections with tysonite crystals, but Templeton and Dauben⁴ found them with a synthetic crystal of CeF₃. The atomic positions given by Oftedal give lanthanum a peculiar coordination geometry with five nearest neighbors and six more neighbors at a greater distance.

We were prompted to study LaF_8 again by the availability of excellent synthetic crystals and recent interest in the spectroscopic properties of ions in this structure. When we had nearly finished the determination of the structure, we learned that Mansmann⁵ had independently reached the same conclusions concerning the symmetry and assignment of atoms to point sets, without reporting atomic coordinates.

We conclude that Oftedal's cell is correct and that his coordinates for La are quite accurate, but that the crystals are trigonal rather than hexagonal. Because of his failure to recognize this point symmetry, Oftedal did not consider the correct space group, and he misplaced most of the F atoms. In our structure, each La is on a twofold axis and has nine neighbors (a normal number) at nearly equal distances.

Experimental Section

A large crystal of lanthanum trifluoride, purported to be 99.999% pure, was sent to us by Dr. Kenneth Lee of Varian

Associates in Palo Alto, Calif. A fragment of this crystal about 0.1 to 0.2 mm in size was glued to the end of a Pyrex fiber with the hexagonal axis parallel to the fiber axis. The crystal was dipped into liquid nitrogen rapidly several times in an attempt to diminish extinction effects by increasing the mosaic spread by thermal shock, but no effect was observed in the intensities before and after the treatment. Diffraction angles and intensities were measured with an Eulerian cradle goniostat equipped with a scintillation counter using Mo K α radiation ($\lambda(K\alpha_1) 0.70926$ A). The cell dimensions measured at 22° are $a = 7.185 \pm 0.001$ and $c = 7.351 \pm 0.001$ A, in excellent agreement with the values reported by Swanson, *et al.*⁶ The density calculated with 6 molecules per cell is 5.938 g/ml.

The diffraction intensities correspond to Laue symmetry $\overline{3}$ m1, but there are clear violations of symmetry 6/mmm and 6/m; *i.e.*, I(hkl) = I(h + k, -k, l), but $I(hkl) \neq I(-k, h + k, l)$. Thus, the crystals are trigonal rather than hexagonal (in the strict sense). The failure of previous workers to recognize the lower symmetry may be the result of twinning in their specimens or the result of low accuracy of intensities estimated from films.

We failed to detect any pyroelectric effect when a large crystal fragment, suspended on a thread, was dipped into liquid nitrogen; when withdrawn, the crystal showed no attraction for the side of the dewar. The systematic absences, (h0l) absent if l = 2n + 1, correspond to space groups P3c1 and P3c1. We conclude that the crystals are centric because a reasonable structure is found in space group P3c1 (D_{8d}^4), No. 165 in the "International Tables."⁷

The intensity measurements included 914 independent reflections (all positive hkl with $2\theta < 90^{\circ}$) of which 63 were recorded as zero. The data were corrected for the Lorentz-polarization effects. The absorption factor μ was estimated to be $\sim 200 \text{ cm}^{-1}$, and the μR for the crystal was estimated to be $\sim 200 \text{ cm}^{-1}$, and the μR for the crystal was estimated to be ~ 2 . The data were not corrected for absorption. An empirical extinction correction was made based on an approximation suggested by Zachariasen[§] where $F_{\rm e} \approx F_{\rm o}(1.0 + CJ)$, where F is the scaled structure factor, J is the raw observed intensity, and C is an adjustable constant.

The structure given by Oftedal² can be fitted to space group $P\overline{3}c1$ by assigning the atoms to point sets as listed in Table I. Prior to the extinction correction, we attempted to refine this structure with a full-matrix, least-squares program, with trialand-error displacements of various atoms to break the higher symmetry. The first set of refinements went poorly; *i.e.*, the R factor, $R = \Sigma ||F_o| - |F_c|| / \Sigma |F_o|$, stayed high (~0.15) and the temperature factor for the twofold fluorine "blcw up." Different trial structures and the use of a noncentric space group (P3c1) gave even worse results. We observed what appeared to be severe extinction effects, and, by deleting some low-angle data which included some of the larger intensities, definite improvement in the refinement resulted. A plot of F_o/F_c (observed and calculated structure factors) vs. the intensities showed a very definite extinction-type correlation. From this plot a value for C in the extinction correction was obtained, and then it was adjusted in the least-squares refinement. The extinction was so severe that the two most intense reflections were observed to be one-eighth of their calculated values. In the final refinements the anomalous dispersion factors for La⁸⁺ were included ($\Delta f' = -0.4$, $\Delta f'' = 2.9$ electrons).⁹ An anisotropic temperature factor of the form $\exp\left[-(h^2\beta_{11}+k^2\beta_{22}+l^2\beta_{33}+2hk\beta_{12}+2hl\beta_{13}+2kl\beta_{23})\right]$ was applied to lanthanum, with suitable constraints because of the twofold axis, and an isotropic temperature factor of the form $\exp[-(B \sin^2 \theta / \lambda^2)]$ was applied to each fluorine. The five most intense reflections and seven of the reflections with the worst

⁽¹⁾ Work done under the auspices of the U. S. Atomic Energy Commission.

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⁽⁵⁾ M. Mansmann, Z. Anorg. Allgem. Chem., 331, 98 (1964).

⁽⁶⁾ H. E. Swanson, N. T. Gilfrich, and M. I. Cook, "Standard X-Ray Diffraction Patterns," National Bureau of Standards Circular 539, Vol. 7, U. S. Government Printing Office, Washington, D. C., 1957, p 21.

^{(7) &}quot;International Tables for X-Ray Crystallography," The Kynoch Press, Birmingham, England, 1952, p 271.

⁽⁸⁾ W. H. Zachariasen, Acta Cryst., 16, 1142 (1963).

⁽⁹⁾ D. T. Cromer, ibid., 18, 17 (1965).

Observed⁴ and Calculated Structure Factors ($\times 2.0$) for Lanthaum Trifluoride^b 53 -52 14 12 14 L0 22 -22 46 -43 5 9 31 28 19 -20 7 -10 8 15 23 20 36 25 16 7 23 205-198 105 107 166 167 96 -95 141-137 76 73 106 105 50 -51 - K# 5 - 7 FDB FCA 0 -2 +8 42 16 18 47 -43 17 -16 37 39 0 -1 34 -34 9 27 24 10 8 11 5 0 -3 6 113-114 7 · 13 1 46 55 33 44 32 -26 -16 14 24 -3 16 55 15 17 36 11 17 36 11 17 -82 155 80 121 -72 100 x = 2, 3FDU FCA 18 10 83 18 40 41 33 34 40 41 33 34 40 -41 33 34 40 -41 33 34 44 -46 44 -46 7 -18 7 -10 7 -1 -36 -270 10112 H,K= 9, 4 L FOB FCA 0 32 -33 1 34 -35 2 20 19 3 23 25 4 17 -20 5 25 -29 7 140-8 73 9 9 105 47 23 36 11 48 16 39 16 7 25 205 199 7 2 8 9 10 11 12 13 H,K# E L F08 0 43 1 7 2 56 1 12 55 0 38 -0 34 191-196 170 174 101-110 1,K= 1, 9 FDB FCA) 25 +28 1 52 -46 1 32 32 1 30 34 3 0 -30 2 2 22 37 35 17 +16 0 -23 H1KF 21 9 L FOB FCA 0 26 24 1 21 -19 2 38 -32 3 28 30 4 28 28 5 22 -22 6 23 -25 7 8 13 8 17 21 8, 3 FCA -5 -53 -53 -34 36 9 10 11 12 13 567 206 208 221-222 174 177 152-153 124 139 91-103 5678901123 132 131 0 -0 H K + 1 L F DB D 33 I 15 2 34 3 29 4 41 5 12 6 33 7 17 8 32 9 13 45678910 0 -3 13 -13 6, 5 FCA 34 -17 -34 29 37 -11 -30 15 33 -19 H₊K= 3,10 L FO6 FCA D 31 -34 1 8 -13 2 25 28 3 6 7 4 13 -20 K 0 F 0B 12 15 15 15 07 3, 4 FCA -59 -22 42 H.K= 5. 8 L FDB FCA 0 55 -62 1 120 119 2 61 62 3 102-108 4 57 -58 5 102 108 10 $\begin{array}{c} \textbf{H}_{4} \textbf{K} = 1, \ \textbf{4} \\ \textbf{L}_{7} \textbf{G} \textbf{U} \textbf{C} \ \textbf{F} \textbf{C} \textbf{A} \\ \textbf{O}_{1} \textbf{C} \textbf{B}_{1} \textbf{C} \textbf{T} \\ \textbf{O}_{1} \textbf{C} \textbf{C} \textbf{S}_{2} \textbf{S}_{4} \\ \textbf{O}_{1} \textbf{S}_{2} \textbf{S}_{4} \textbf{C} \\ \textbf{S}_{1} \textbf{S}_{2} \textbf{S}_{4} \\ \textbf{S}_{1} \textbf{S}_{2} \textbf{S}_{4} \\ \textbf{S}_{1} \textbf{S}_{2} \textbf{S}_{4} \\ \textbf{S}_{1} \textbf{S}_{1} \textbf{C} \textbf{S}_{4} \\ \textbf{S}_{1} \textbf{S}_{1} \textbf{S}_{1} \\ \textbf{S}_{1} \textbf{S}_{2} \\ \textbf{S}_{1} \textbf{S}_{2} \textbf{S}_{4} \\ \textbf{S}_{1} \textbf{S}_{1} \textbf{S}_{1} \\ \textbf{S}_{1} \textbf{S}_{2} \\ \textbf{S}_{1} \textbf{S}_{1} \textbf{S}_{2} \\ \textbf{S}_{1} \textbf{S}_{2} \\ \textbf{S}_{1} \textbf{S}_{2} \textbf{S}_{4} \\ \textbf{S}_{1} \textbf{S}_{1} \textbf{S}_{2} \\ \textbf{S}_{1} \textbf{S}_{2} \\ \textbf{S}_{2} \textbf{S}_{1} \\ \textbf{S}_{2} \textbf{S}_{2} \\ \textbf{S}_{1} \textbf{S}_{2} \\ \textbf{S}_{2} \textbf{S}_{2} \\ \textbf{S}_{1} \textbf{S}_{2} \textbf{S}_{2} \\ \textbf{S}_{2} \textbf{S}_{2} \\ \textbf{S}_{1} \textbf{S}_{2} \textbf{S}_{2} \\ \textbf{S}_{2} \textbf{S}_{2} \\textbf{S}_{2} \\ \textbf{S}_{2} \textbf{S}_{2} \\ \textbf{S}_{2} \textbf{S}_{2} \textbf{S}_{2} \\ \textbf{S}_{2} \textbf{S}_{2} \\textbf{S}_{2} \\ \textbf{S}_{2} \textbf{S}_{2} \\textbf{S}_{2} \\ \textbf{S}_{2} \textbf{S}_{2} \\textbf{S}_{2} \\ \textbf{S}_{2} \textbf{S}_{2} \\textbf{S}_{2} \\ \textbf{S}_{2} \textbf{S}_{2} \textbf{S}_{2} \\textbf{S}_{2} \\ \textbf{S}_{2} \textbf{S}_{2} \\textbf{S}_{2} \\textbf{S}_{2} \\ \textbf{S}_{2} \textbf{S}_{2} \textbf{S}_{2} \ \textbf{S}_{2} \\textbf{S}_{2} \\textbf{S}_{2} \\textbf{S}_{2} \\textbf{S}_{2} \ \textbf{S}_{2} \textbf{S}_{2} \textbf{S}_{2} \textbf{S}_{2} \ \textbf{S}_{2} \ \textbf{S}_{2} \textbf{S}_{2} \ \textbf{S}_{2}$ H+K* 3, 4 L FOB FCA 0 53 -659 1 21 -22 2 44 42 5 29 -22 5 29 -22 6 25 23 7 11 14 8 25 -21 9 7 -7 10 0 7 -7 11 13 13 12 23 -20 02468 1012 FD8 FCA 32 26 13 -15 5 67 8 9 H.K= 0.10 L 20B FCA 0 45 -43 2 35 35 4 19 -16 6 20 24 6 20 -21 K= 7. 4 F08 FCA 73 -74 163-163 85 84 151 145 87 -86 138-132 71 70 H K = L F08 0 10 1 76 2 27 3 40 4 25 1 22 6 4 9 -0 24 0 15 -1 0 20 2 2+ 4 3 FCA 5 F H.K= 4, 0 L FDB FCA 2 11 -4 4 78 -73 6 37 37 8 0 7 10 26 17 12 17 +10 K* 8, 4 FD8 FCA 0 7 43 -39 7 -2 31 33 8 -9 30 -33 H,K= 1,10 L FOB FCA 0 62 -66 1 130-129 2 71 77 3 125 124 4 65 -68 5 126-126 6 60 63 7 84 97 H,K= 2,10 L FOB FCA 0 13 -15 1 41 40 2 23 25 3 37 -40 4 20 -23 5 38 39 6 13 12 H,K= 0, 2 L f08 FCA 0 34 26 2 40 39 4 38 38 6 19 -2L 8 16 18 10 26 -3L 12 7 18 14 0 -6 42 34 45 -44 35 35 22 -20 H.K. 5, 9 L FOB FEA D 28 26 L 17 -13 H.K= 0.11 L COB FCA 0 42 42 2 45 46 4 43 40 6 34 -37 .K: 6, 6 FDB FCA 156 154 12 =4 158-167 7 -4 4, 6 -41 33 -39 -32 34 29 -16 -15 16 K= ' FOB 45 20 320 320 320 337 20 337 20 6 10 12 14 K* 6, 0 FD8 FCA 325-316 296 293 249-239 191 181 157-153 114 120 126 120 69 -67 95 -94 11 12 13 $\begin{array}{c} 12 \quad 17 \quad -10 \\ \text{H}, \text{Ke} = 4, \ 1 \\ \text{L} \quad \text{FOB} \quad \text{FCA} \\ 0 \quad 173 \quad 175 \\ 1 \quad 333 \quad 332 \\ 2 \quad 151 \quad 149 \\ 3 \quad 348 \quad 340 \\ 4 \quad 162 \quad 157 \\ 5 \quad 262 \quad 251 \\ 6 \quad 161 \quad 153 \\ 7 \quad 220 \quad 214 \\ 8 \quad 116 \quad -114 \\ 116 \quad 112 \\ 125$ 8 \$ 3. 5 FCA 37 -15 -32 -28 52 -23 125 -23 125 -15 -40 322 3 7 -4 4 153 150 5 7 -3 6 118-123 7 8 2 F 4 745542057708 - 72 - 72 - 72 - 48 - 10 - 14 - 14 - 14 - 14 - 12 H.K= 1.5 FOS FCA U 29 29 1 16 4 29 29 2 32 -33 3 49 -52 4 16 15 3 49 -52 4 16 15 5 47 45 6 36 -37 10 -6 8 11 17 9 29 29 1 16 4 1 17 45 6 36 -37 1 0 -6 8 11 17 2 8 5 3 0 4 F08 35 16 36 27 55 34 11 32 19 44 20 K= 7, 5 FUB FCA 0 ~2 41 43 13 12 39 -40 0 -6 30 -6 30 -30 H,K= 2,ll L FOB FCA 0 49 -53 1 96 100 2 52 58 68 122 K= 8, 5 FOB FCA 60 -62 122 124 5, 58 106-107 M,K* 0, 3 L F0B FCA 0 713 678+ 2 659-677 4 350 380+ 6 338-357 8 221 235 10 177-182 12 158 158 14 99-105 H₁K* 1,11 L-F08 FGA 0 13 13 1 32 28 2 13 -16 3 28 -27 4 17 15 5 25 26 5 112-112 6 60 62 7 103 109 10 12345678901123 6, 7 FCA -38 -24 120 -22 -22 -22 H, K= 2, 5 H, K= 2, 5 L FOB FCA 0 134-138 1 260 260 2 124 132 3 253-253 4 123-124 5 223 222 6 128 124 7 180-178 8 103-100 9 149 148 10 75 75 11 116-115 12 60 -57 K= 6 FOB 23 25 17 23 25 17 23 20 H+K× 1 L FOB 2 L4 4 47 6 9 8 9 10 0 12 7 14 0 H K= 3, 0 L FOB FCA 2 496-469 4 373 386 6 350-357 8 226 228 10 177-184 12 163 157 14 97-105 5.67890112 DA 36444 10 58 -62 K=10, 2 FOB FCA 4567 K* 4, 7
f08 FCA
68 -74
155-154
87 88
145 146
83 -82
138-139
74 70
119 114
59 -69
54 13 45 136 32 0 -15 48 -38 -13 -13 -13 -13 8 9 10 11 12 H,K= 8, 6 L FDB FCA 0 36 34 1 13 -10 2 36 -37 H,K= 2, 0 L F0B FCA 2 114-108 4 37 41 6 43 -48 8 32 35 10 0 -3 12 7 3 14 8 -4
 7
 30
 -30

 H,K=
 7.6
 6

 L
 F08
 FCA

 0
 37
 -38

 1
 29
 -26

 2
 34
 34

 3
 13
 17

 4
 31
 -31

 5
 20
 -24

 6
 30
 31
 H.K= 04 4 L F38 FCA 0 58 -68 2 46 48 4 64 44 6 20 17 8 24 -20 10 0 2 12 22 -19 $\begin{array}{c} \text{H}, \text{K} \approx 3, \ 6\\ \text{L} \ \text{FOB} \ \text{FCA} \\ 0 \ 256 \ 252 \\ 1 \ 0 \ -3 \\ 2 \ 258 - 254 \\ 3 \ 6 \ -4 \\ 217 \ 213 \\ 5 \ 7 \ -3 \\ 6 \ 184 - 180 \\ 184 - 180 \\ 7 \ 12 \ 2 \\ 8 \ 160 \ 152 \\ 9 \ 0 \ 2 \\ 10 \ 119 - 120 \\ 11 \ 0 \ 1 \end{array}$ H, Ka 4, 2 L F08 FCA 0 10 6 1 23 17 2 10 8 3 40 -42 4 11 8 5 55 5 5 55 -5 17 -20 7 18 -14 8 6 -4 9 24 23 10 0 6 11 24 -23 10 0 -42 13 8 7 FCA 34 -37 FCA 580 -401 -411 -20 FDB 32 0 33 $\begin{array}{c} 14 & 97 - 103 \\ H, K = 3, 1 \\ i \ FOB \ FCA \\ 0 \ 32 \ -35 \\ i \ 6 \ 2 \ 26 \ 28 \\ 3 \ 17 \ 16 \\ 4 \ 33 \ 37 \\ 5 \ 43 \ -5 \ -4 \\ 6 \ 5 \ -4 \\ 6 \ 5 \ -4 \\ 6 \ 5 \ -4 \\ 15 \ -11 \\ 10 \ 7 \ 3 \\ 11 \ 12 \ 16 \\ 10 \ 7 \ -13 \\ 11 \ 0 \ -4 \end{array}$ 56789 FOB 10 60 16 47 11 32 7 46 31 0 17 S = 10, 3 OH FCA 3L - 34 8 - 12 32 34 8 8 37 - 34 F 38 324 454 174 483 191 272 H,K= 1, 6 L F08 FCA 0 26 -31 1 50 -62 2 28 29 3 26 28 3 9 -43 5 33 -33 5 20 22 7 43 41 8 12 -9 9 19 -19 10 13 12 11 20 19 12 8 -7 FCA 234 426 166 537 183 305 1 H K = L FUB D 20 1 82 3 35 3 35 4 9 6 13 7 3 7 8 4 9 18 9 18 9 0 13 0 0 13 H,Ka 2, 6 L FOB FCA 0 31 32 1 10 -6 2 54 -51 3 35 43 2 52 6 -27 6 37 -37 7 7 5 8 29 30 9 .19 -23 10 7 -10 11 13 12 H.K= 7, 0 L FOB FCA 2 25 22 4 51 -59 6 47 44 8 14 -9 10 18 24 12 15 -18 H, K* 4, 8 L FOB FCA 0 0 9 1 36 36 2 0 -3 3 36 -36 4 7 4 5 34 32 6 8 -13 7 25 -25 2, 1 FCA 20 36 -38 -38 -13 -35 10 17 -16 -5 11 H.K# /, 7 L FUB FCA 0 49 -51 1 97-L03 2 49 58 H,K= 0, 5 L, FDB FCA 0 26 34 2 23 -15 4 62 63 6 27 -31 8 31 32 10 41 -44 12 13 21 5678901 44 - 44 25 - 28 44 - 44 21 22 27 32 7 - 16 H+K+11, 0 L FOB FCA 2 54 -48 4 54 50 6 36 -39 8 129-133 9 222-228 10 131 130 11 140 142 12 18 -80 13 137-138 14 49 47 10 H.K. E. 0 L FDB FCA 2 63 -69 4 60 55 6 42 -43 8 45 43 0 24 -24 H,K= 5, 5 L FDB FCA 0 95 -99 1 190 189 2 86 92 3 165-167 4 92 -92 5 165 160 6 92 88 7 136-136 8 74 -73 9 106 166 0 54 56 3, 7 FCA -50 -19 35 8 7 -16 47 -38 13 13 31 30 13 -14 17 -20 FOB 46 14 36 7 H, K# 4, 3 L FOB FCA 0 53 -59 1 38 -38 2 21 19 3 59 -59 5 17 -20 6 39 39 7 24 24 8 7 -6 9 7 -8 10 24 24 10 7 -8 10 24 24 10 7 -8 10 24 24 10 7 -8 10 24 24 10 7 -8 10 24 24 10 7 -8 10 24 24 10 7 -8 10 24 24 10 7 -8 10 24 24 10 7 -8 104-10, 233-231 107 107 8 10 FOR FCA 13 13 34 33 8 -8 34 -30 8 11 28 27 H,K≈ 0, 6 L FDB FCA 0 366 360 2 310-339 4 270 274 6 233-241 8 191 191 10 139-145 12 116 121 67 8 9 H, Ka 4, 9 L FOB FCA O 34 -33 1 37 -34 2 36 33 3 23 26 4 23 -25 5 28 -32 10 11 12 13 14 H+K= 3, 2 L F0B FCA 0 32 34 1 43 -42 2 20 9 3 39 41 4 50 47 5 5 6 20 -28 8 20 22 9 21 -19 10 33 -36 11 0 33 12 17 19 13 8 -11 10 209 204 118-116 195-176 100 99 170 162 91 -84 130-124 72 70 103 96 FDB 19 31 42 36 28 42 32 9 6 16 0 15 7 0 -12 -18 26 13 -20 H.K. 8 0 23 1 46 2 46 3 44 4 11 5 28 6 27 8 7 K= 0, 1 FOB FCA 23 22 46 4-2 44 -44 11 13 28 23 20 -19 37 -36 7 11 31 28 13 -17 15 21 28 20394 2, 7 5 FCA 5 56 5 56 5 - 43 5 - 27 3 5 - 27 3 6 H,K= 6, 3 i, F08 FCA 0 259 252 l 6 -3 2 252-241 3 6 -4 4 235 225 5 11 -3 6 190-179 7 12 2 8 158 148 9 7 2 H, Ka Z, Z H, Ka Z, Z L F08 FCA C 218-218 1 366 370 2 158 160 2 158 160 2 420-4114 4 165-166 2 69 279 6 183 179 7 224-230 6 183 179 7 224-230 6 122-123 9 206 201 10 95 93 13 103 134 12 79 -73 13 104 102 14 42 45 8 22 -20 9 8 -6 10 13 13 51 0 FCA -98 46 -47 -13 10 0, 7 FCA 45 29 -24 H,K× 0, 7 L FDB FCA 0 54 -62 2 44 45 4 13 6 6 28 29 B 27 -24 10 7 8 12 20 -22 H 1 2 4 6 8 10 2 FDB 101 50 45 49 14 11 1 106 111 2 48 50 15 17 -15 -12 2 3. B FCA 40 -4 -44 16 43 5, 6 FCA -10 -47 -27 -12 -34 K= F08 41 44 10 47 K= 7 F08 6 46 16 39 0 46 7 33 15 F 49184591 10 11 12 13 14 -41 -10 28 6 H,K=12. D L FOB FCA 2 115-119 9 10 9 10 H.K* L. 8 L FDB FCA 0 23 22 L 24 23 2 23 -22 J 4L -4L 4 18 15 10 131-126 H.K= 8. 2 FCA 152 K* FOB FC B3 -86 167 166 84 92 K= 3, 3 FOB FCA 430 423 B -3 H,K= 5, 1 L FDB FCA O 27 29 1 68 66 2 L7 L8 33 0 36 84 1 182 2 83 3 158-+K= 1, 3 FUB FCA 32 -35 57 -69 01 1 239-2+0 2 123 124 3 235 229 4 122-122 K 6. 4 FDB FCA 43 -44 34 -36 183 82 H.K= 0. 6 L FDB FCA 0 41 41 0 7 7 36 31 13 -15

TABLE I

^a The observed FOB = $S\sqrt{JL\rho}(1.0 + CJ)$, where S is the over-all scaling factor from least squares of 10.826, J is the raw intensity corrected for background, Lp is the Lorentz-polarization correction, and C is the extinction correction factor of 0.000464. ^b The asterisked data in the FCA column are those given zero weighting in the least-squares calculation.

8

1

TABLE II

POSITIONAL PARAMETERS IN LANTHANUM TRIFLUORIDE

No.	Atom	Point symmetry	Positions and postional parameters	
6	La	2	$\pm (x, 0, \frac{1}{4}; 0, x, \frac{1}{4}; \tilde{x}, \tilde{x}, \frac{1}{4})$	
12	F(1)	1	$ \begin{array}{l} x = 0.3401 \pm 0.0005 \\ \pm(x, y, z; \ \bar{y}, x - y, z; \ y - x, \bar{x}, z; \\ \bar{y}, \bar{x}, \frac{1}{2} + z; \ x, x - y, \frac{1}{2} + z; \\ y - x, y, \frac{1}{2} + z; \end{array} $	
			$x = 0.312 \pm 0.002$ $y = -0.005 \pm 0.002$ $z = 0.581 \pm 0.002$	
4	F(2)	3	$\pm (1/_{3}, 2/_{3}, z; 1/_{3}, 2/_{3}, 1/_{2} + z)$	
2	F(3)	32	$z = 0.313 \pm 0.002$ $\pm (0, 0, \frac{1}{4})$	

TABLE III

Temperature Factors $(A^2)^{\mathfrak{a}}$ in Lanthanum Trifluoride							
Atom	Temp factors						
La	$B_{11} = 0.6 \pm 0.2$	$B_{22} = 0.6 \pm 0.2$	$B_{33} = 0.8 \pm 0.2$				
	$B_{12} = 0.3^{b}$	$B_{13} = -0.025^{b}$	$B_{23} = -0.05 \pm 0.01$				
F(1)	$B = 1.3 \pm 0.4$						
F(2)	$B = 1.0 \pm 0.4$						
$\mathbf{F}(3)$	$B = 1.7 \pm 0.7$						

^a Anisotropic $B_{ij} = \beta_{ij}/4a^*_i a^*_j$, where a^*_i is the *i*th reciprocal axis length. ^b Symmetry considerations force $B_{22} = 2B_{12}$ and $B_{23} = 2B_{12}$ $2B_{18}$.

agreement were deleted from the final refinements. The final Rfactor was 0.052. The observed and calculated structure factors are shown in Table I.

Results

Tables II and III show the final positional and thermal parameters, respectively. The standard deviations shown in Tables II and III are estimates by the authors rather than the results of the least squares and in all cases are considerably larger than the calculated values. These estimates resulted from a study of the parameters as conditions of the refinement were modified. The parameters changed considerably more



Figure 1.--The ninefold coordination of lanthanum in lanthanum trifluoride as viewed down the c axis.

TABLE IV Interatomic Distances of Less Than 3 A in Lanthanum Trifluoride

	Distance,		Distance,
Atoms	A	Atoms	A
La-2F(2)	2.416 ± 0.003	F(1)-1F(2)	2.69 ± 0.02
La-1F(3)	2.443 ± 0.004	F(1)-2F(1)	2.74 ± 0.02
La-2F(1)	2.46 ± 0.02	F(1)-1F(3)	2.76 ± 0.01
La-2F(1)	2.49 ± 0.01	F(1)-1F(2)	2.79 ± 0.01
La-2F(1)	2.64 ± 0.01	F(1)-1F(2)	2.87 ± 0.02
La-2F(1)	3.01 ± 0.01	F(2)- 3 La	2.416 ± 0.003
F(1)–1La	2.46 ± 0.02	F(2)-3F(1)	2.69 ± 0.02
F(1)-1La	2.49 ± 0.01	F(2)-3F(1)	2.79 ± 0.01
F(1)-1La	$2.64 \hspace{0.2cm} \pm \hspace{0.2cm} 0.01 \hspace{0.2cm}$	F(2)-3F(1)	2.87 ± 0.02
F(1)-1La	3.01 ± 0.01	F(3)–3La	2.443 ± 0.004
F(1) - 1F(1)	2.57 ± 0.03	F(3)-6F(1)	2.76 ± 0.01
F(1)-1F(1)	2.68 ± 0.03		

than the calculated standard deviations when just high-angle data were used or when the extinction correction was introduced. Our estimates of the standard deviations bracket these fluctuations more realistically, and, because of the highly nonrandom nature of the errors here, the authors believe that an educated guess is preferable to a mathematical fiction. The thermal parameters (other than B_{13} and B_{23}) are systematically lower than the true values, because of neglect of absorption, by an unknown amount which is estimated to be about 0.6 A^2 . This effect is not included in the estimated standard deviations. Table IV shows a list of interatomic distances.

The structure we find has lanthanum in almost exactly the positions reported by Oftedal. The fluorine atoms have been shifted so that of the six second-nearest neighbors of each lanthanum, four have moved closer and two have moved away; thus, lanthanum has a normal coordination number of nine. We have failed to find any simple description for the geometry of these neighbors. Each fluorine has three lanthanum neighbors. A sketch showing the ninefold coordination of lanthanum as viewed down the *c* axis is shown in Figure $1.^{10}$

(10) NOTE ADDED IN PROOF.—M. Mansmann, Z. Krist., **122**, 375 (1965), has recently reported atomic coordinates for this structure which correspond to our results within 0.06 A in the worst case and with complete agreement concerning the symmetry.

Contribution from the Department of Chemical Engineering, The University of Texas, Austin, Texas

The Structure of YbSb₂, a ZrSi₂ Isotype¹

BY R. WANG, R. BODNAR, AND H. STEINFINK

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In the recent study of the ytterbium-antimony phase diagram,² YbSb₂ was found to exist as one of the most stable phases in this system. It crystallizes in a pro-

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⁽²⁾ R. E. Bodnar and H. Steinfink, Fifth Rare Earth Research Conference Preprints, Iowa State University, Ames, Iowa, 1965.